

NTEC 2014	1	Lecture CFD-3
	31	

CFD modelling of multiphase flows

Simon Lo
CD-adapco
Trident House, Basil Hill Road
Didcot, OX11 7HJ, UK
simon.lo@cd-adapco.com

NTEC 2014	2	Multiphase models and applications
	31	

- VOF
 - Free surface flows
- LMP
 - Droplet flows
 - Liquid film
- DEM
 - Particle flows
- EMP
 - Particle flows
 - Bubbly flows
 - Population balance
 - Boiling heat and mass transfers
 - Interphase mass transfer

NTEC 2014	3 31	Volume of Fluid (VOF) model
--------------	---------	------------------------------------

- Solve equation for volume fraction (based on conservation of mass) to identify location of gas and liquid.

$$\frac{\partial \alpha_i}{\partial t} + \nabla \cdot (\alpha_i u) = \dot{m}_i$$

- Momentum equation for the gas-liquid mixture:

$$\frac{\partial}{\partial t} (\rho_m u_i) + \frac{\partial}{\partial x_j} (\rho_m u_j u_i - \tau_{ij}) = -\frac{\partial p}{\partial x_i} + \rho_m g_i + M$$

- Properties of mixture:

$$\rho_m = \sum_{i=1}^N (\alpha_i \rho_i)$$

$$\mu_m = \sum_{i=1}^N (\alpha_i \mu_i)$$

Gas flow

Liquid

NTEC 2014	4 31	Slug flow in interconnected subchannels
--------------	---------	--

Calculation grid 204,512 cells

20 mm

150 mm

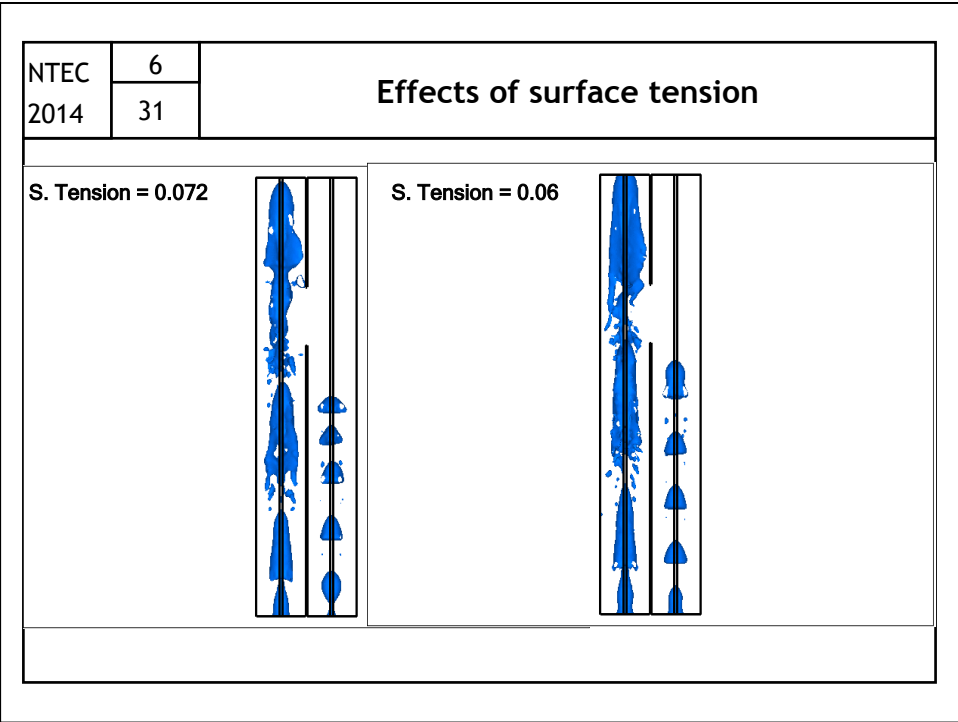
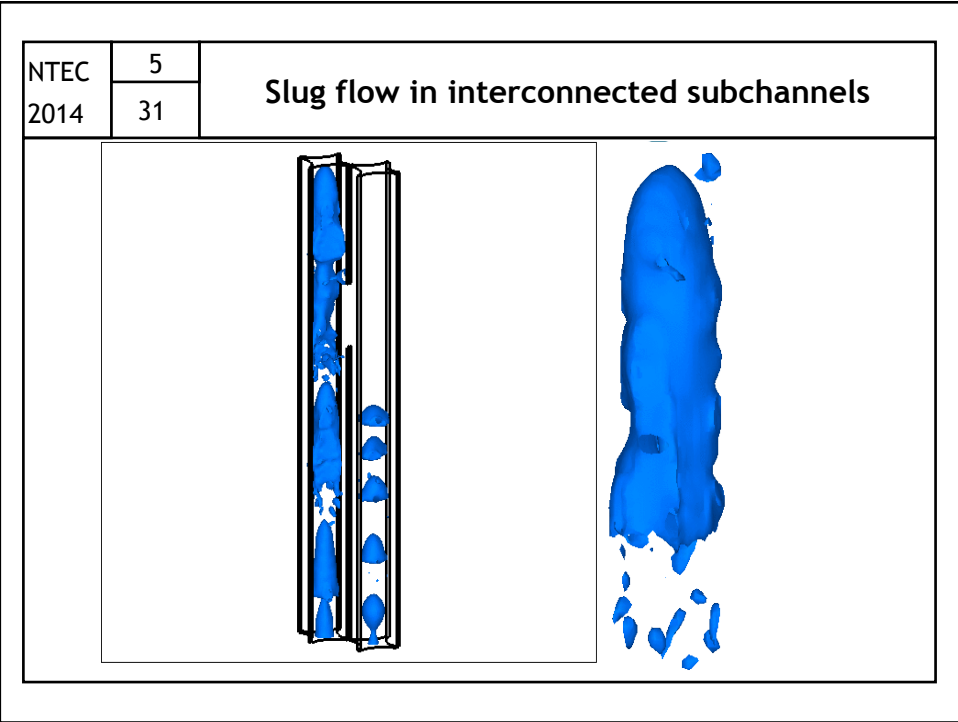
18.7 mm

1.7 mm

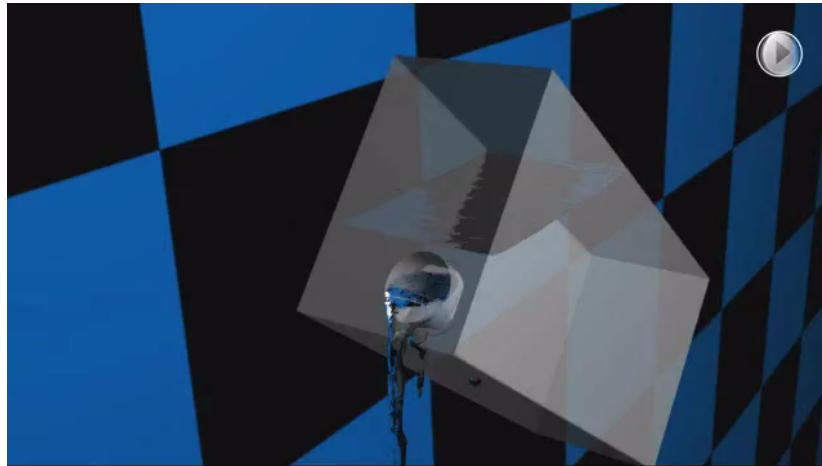
Water Inlet 0.23 m/s

Air Inlet 2.0 m/s

Air Inlet 0.5 m/s



NTEC 2014	7	Free surface flow in drink carton
	31	

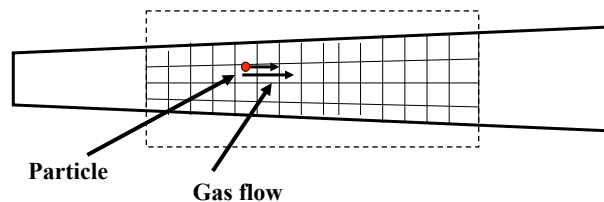


NTEC 2014	8	Lagrangian model for particle flows
	31	

- Equation of motion for individual particle:

$$m_d \frac{du_d}{dt} = F \quad u_d = \frac{dx_d}{dt}$$

- F = force acting on particle



NTEC	9
2014	31

Spray modelling

- Modified Han et al atomisation model

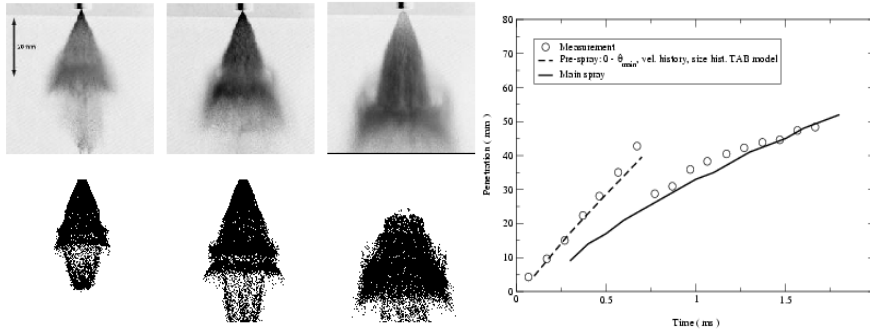
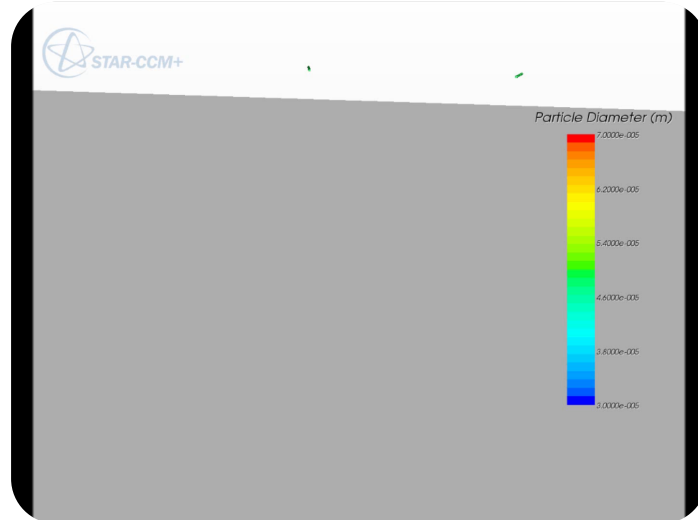


Figure 1: Atm spray images - predictions, at 0.8 ms, 1.2 ms, 1.7 ms, injector
 Bosch 60°/0° injection pressure 5 MPa, injection duration 1.5 ms

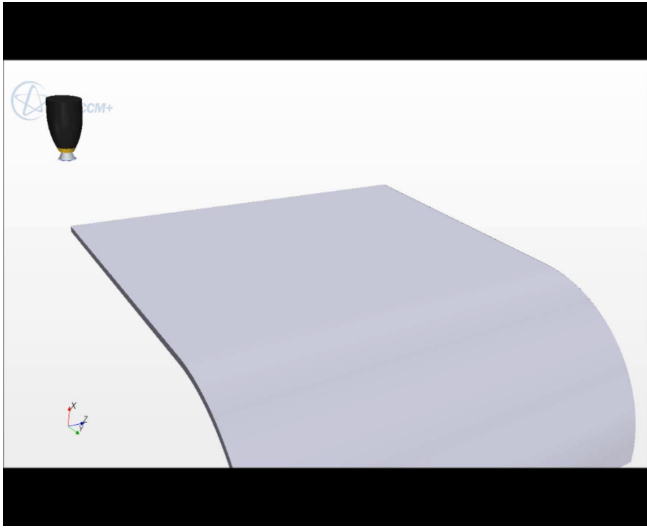
Charalambos (2002)

NTEC	10
2014	31

Droplet collision and coalescence



NTEC 2014	11	Spray coating
	31	

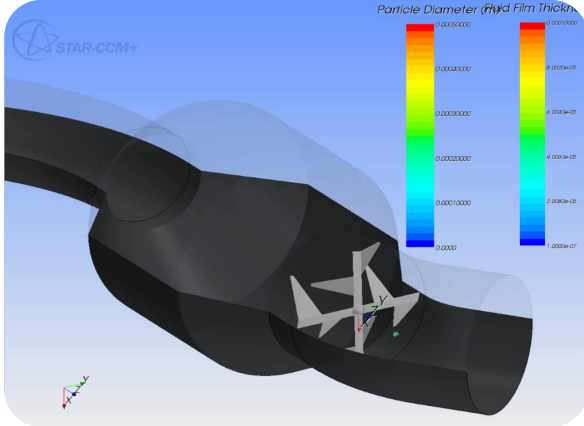


A 3D simulation showing a spray nozzle at the top left, emitting a spray of particles onto a curved, light-colored surface. The spray is depicted as a cloud of small particles. The simulation is set against a white background with a black top and bottom border. A small 3D coordinate system is visible in the bottom left corner of the simulation area.

NTEC 2014	12	Fluid film boiling
	31	

Simulation of films and their evaporation on high temperature surfaces

- Walls above saturation temperature of droplet fluid
- Required multi-component film

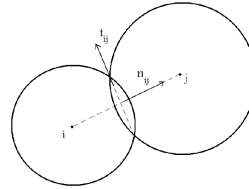


A 3D simulation showing a complex, dark-colored geometry with a fluid film boiling on its surface. The simulation is set against a light blue background. A color scale legend is visible on the right side of the image, with two columns: 'Particle Diameter (μm)' and 'Film Thickness'. The 'Particle Diameter' scale ranges from 0.0000000 to 0.0000000, and the 'Film Thickness' scale ranges from 0.0000000 to 0.0000000. A small 3D coordinate system is visible in the bottom left corner of the simulation area.

NTEC 2014	13	DEM (Discrete Element Method)
	31	

- Linear momentum of particle:

$$m_i \frac{d\vec{v}_i}{dt} = \vec{F}_{Drag} + \vec{F}_{Contact} + \vec{F}_{Other}$$

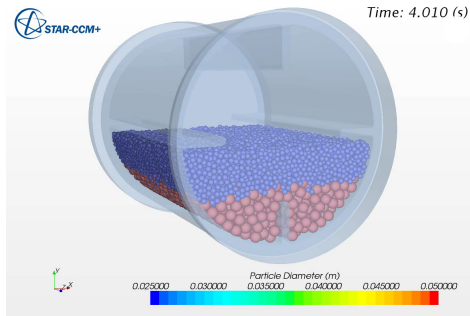


- Angular momentum:

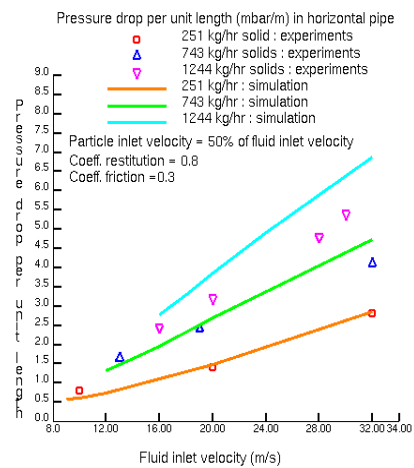
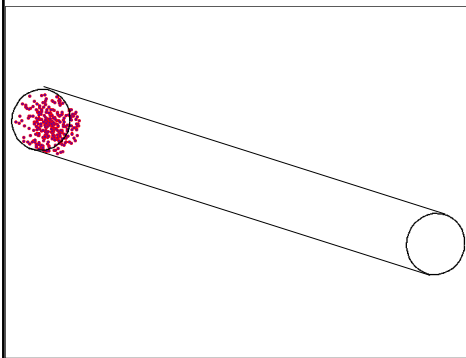
$$I_i \frac{d\vec{\omega}_i}{dt} = \sum_{j=1}^k [\vec{r}_{ij} \times \vec{M}_{ij}]$$

$$\vec{M}_{ij} = -\mu_{roll} |\vec{F}_{Contact}| \vec{\omega}_i$$

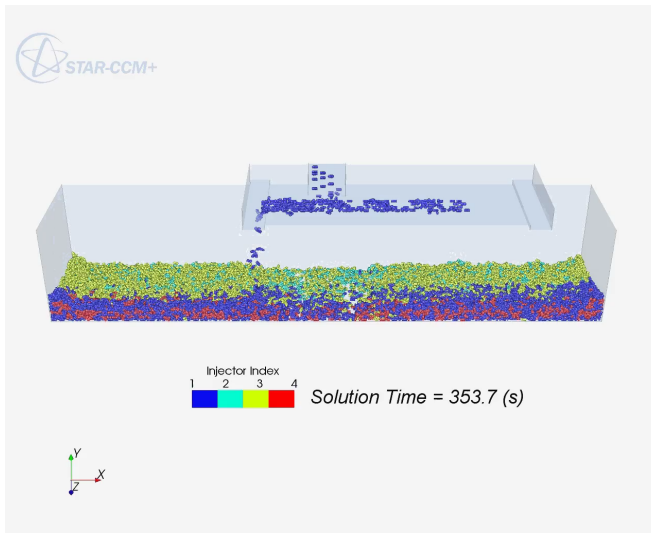
- \vec{M}_{ij} = rolling torque
- μ_{roll} = rolling friction coefficient.



NTEC 2014	14	Pneumatic conveying of particles in pipe
	31	



NTEC 2014	15	Spreading of particles by conveyor belts
	31	



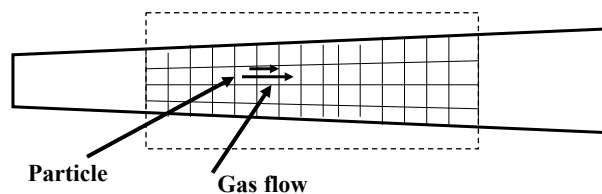
NTEC 2014	16	Eulerian multiphase model
	31	

- Conservation of mass of phase k:

$$\frac{\partial}{\partial t} (\alpha_k \rho_k) + \nabla \cdot (\alpha_k \rho_k \mathbf{u}_k) = \sum_{j=1}^N (\dot{m}_{jk} - \dot{m}_{kj})$$

- Conservation of momentum of phase k:

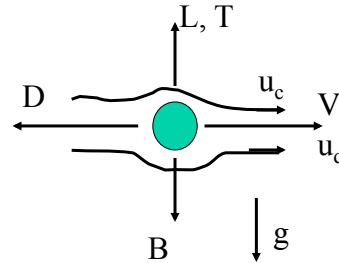
$$\begin{aligned} & \frac{\partial}{\partial t} (\alpha_k \rho_k \mathbf{u}_k) + \nabla \cdot (\alpha_k \rho_k \mathbf{u}_k \mathbf{u}_k) \\ &= -\alpha_k \nabla p + \alpha_k \rho_k \mathbf{g} + \nabla \cdot \alpha_k (\boldsymbol{\tau}_k + \boldsymbol{\tau}_k^t) + M_k \end{aligned}$$



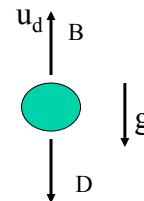
NTEC	17
2014	31

Forces on a particle

- Forces acting on a particles:
 - Buoyancy, B.
 - Drag, D.
 - Lift, L.
 - Virtual mass, V.
 - Turbulent dispersion, T.
 - Basset force.
 - And others.

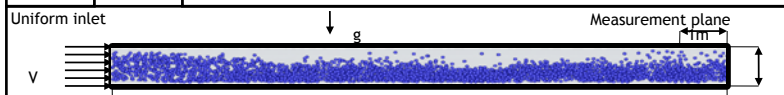


- Buoyancy and drag are the dominant ones.
- Basset force is complicated and almost always ignored. Lift, virtual mass and other forces will be considered later.

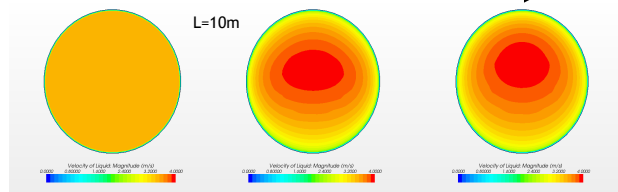


NTEC	18
2014	31

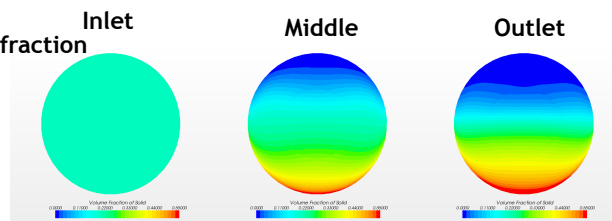
Slurry flow in horizontal pipe

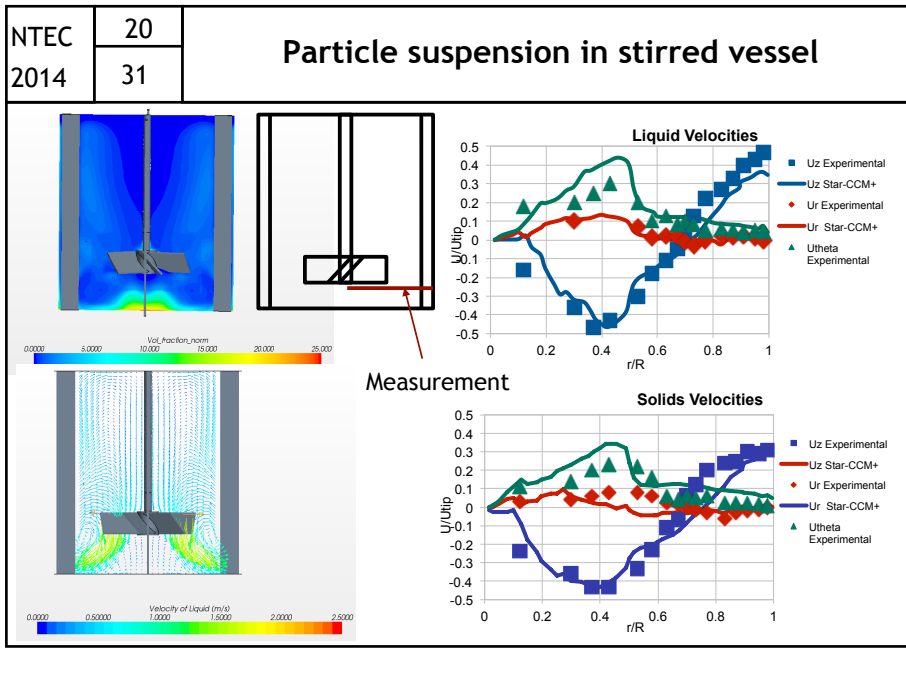
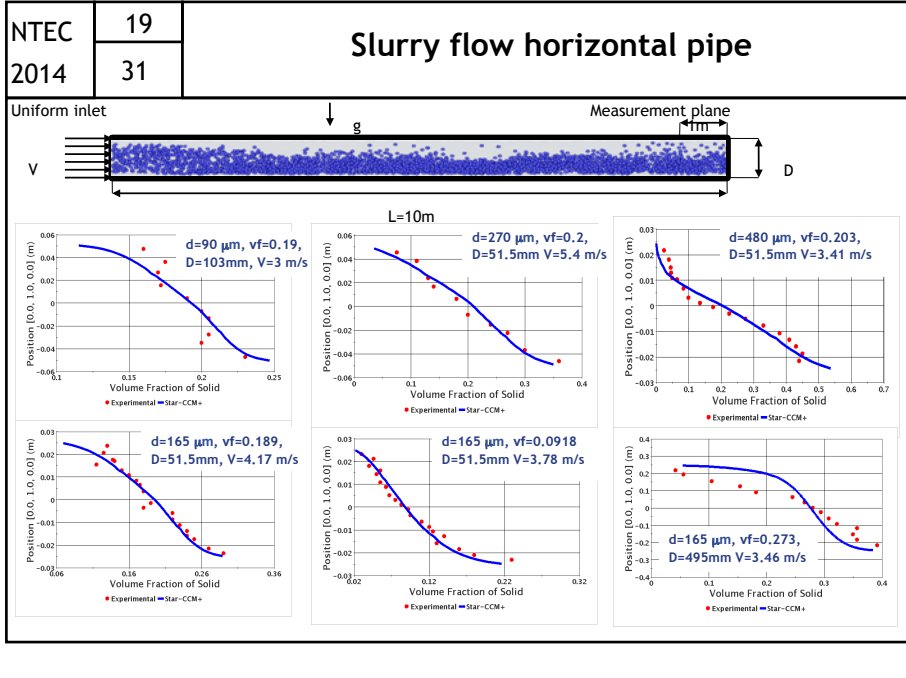


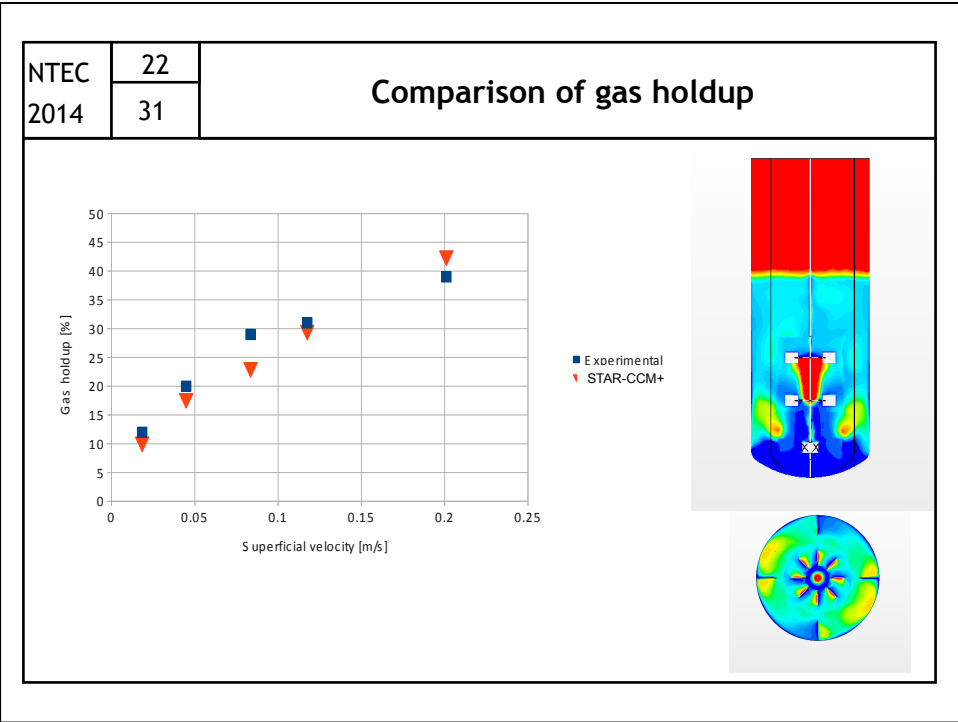
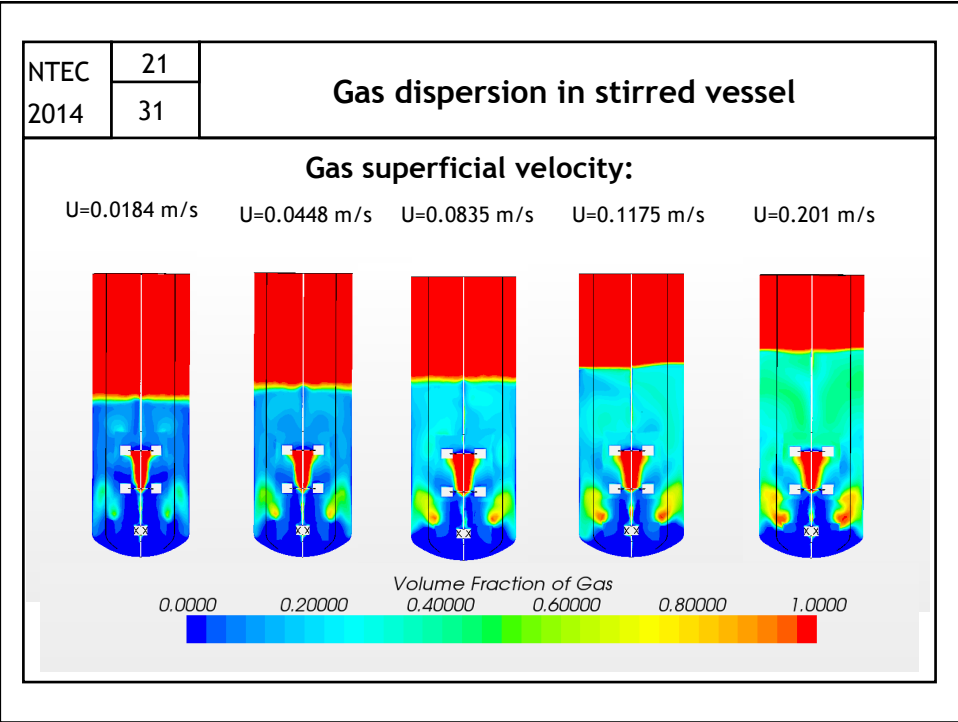
Liquid velocity



Particle volume fraction







NTEC	23
2014	31

Adaptive MUSIG Model

An Eulerian population balance method for poly-disperse multiphase flows.

$$\frac{\partial \alpha_i \rho_i}{\partial t} + \nabla \cdot (\alpha_i \rho_i \mathbf{u}_i) = \sum_{i \neq j} (m_{ij} - m_{ji}),$$

$$\frac{\partial \alpha_i \rho_i \mathbf{u}_i}{\partial t} + \nabla \cdot (\alpha_i \rho_i \mathbf{u}_i \mathbf{u}_i) = -\alpha_i \nabla P + \sum_{i \neq j} (m_{ij} \mathbf{u}_j - m_{ji} \mathbf{u}_i) + \mathbf{F}_i.$$

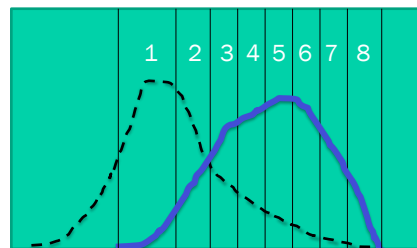
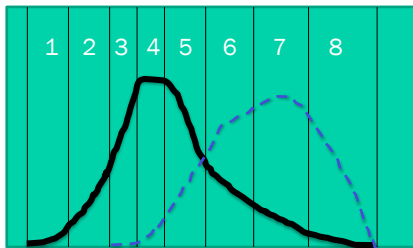
$$\frac{\partial n_i}{\partial t} + \nabla \cdot (n_i \mathbf{u}_i) = S_i,$$

$$d_i = \sqrt[3]{(6\alpha_i)/(\pi n_i)}.$$

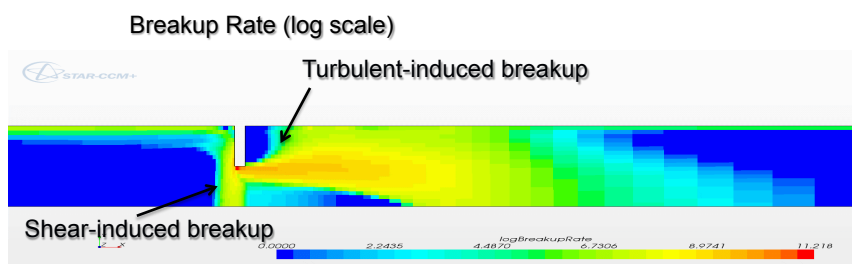
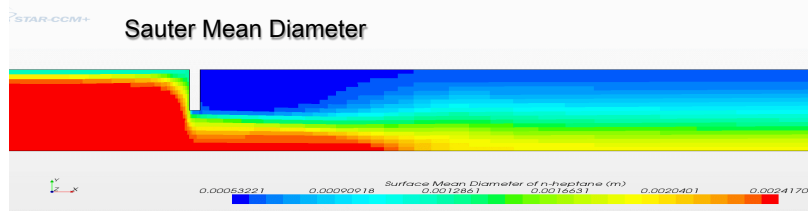
NTEC	24
2014	31

Adaptive MUSIG Model

Mass and number density are redistributed between neighbour groups so that each group has the same mass but new diameters.



NTEC 2014	25	Droplet breakup through an orifice
	31	



NTEC 2014	26	Boiling heat and mass transfers
	31	

- Conservation of energy for phase k:

$$\frac{\partial}{\partial t}(\alpha_k \rho_k h_k) + \nabla \cdot (\alpha_k \rho_k u_k h_k) - \nabla \cdot \left[\alpha_k \left(\lambda_k \nabla T_k + \frac{\mu_t}{\sigma_h} \nabla h_k \right) \right] = Q_k$$

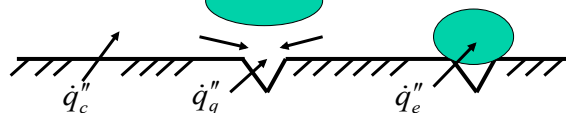
- Wall heat flux is modelled by three mechanisms:

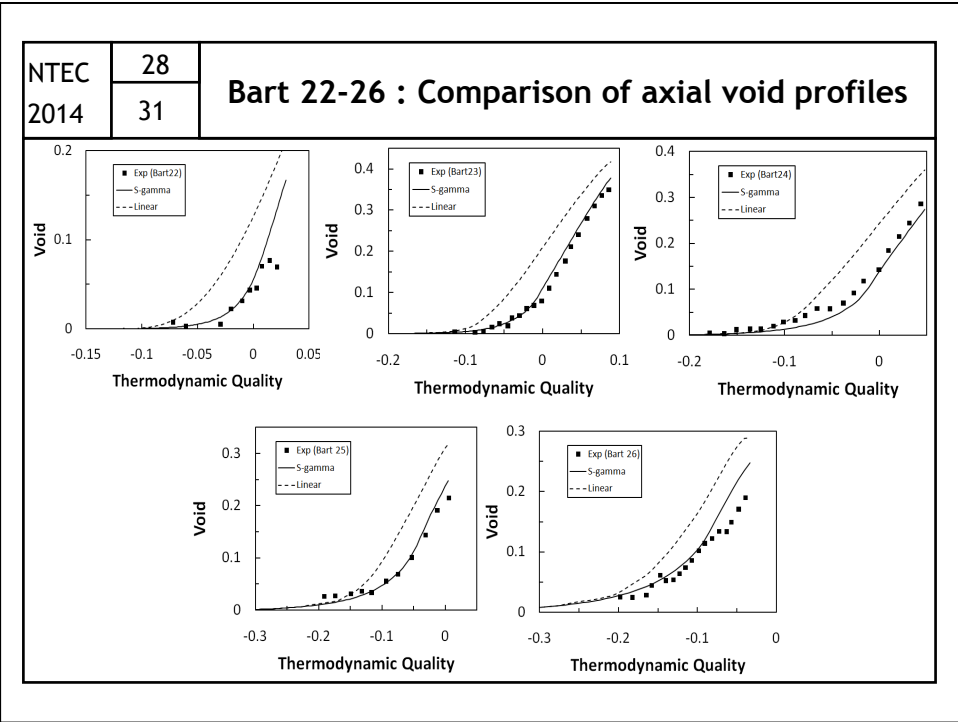
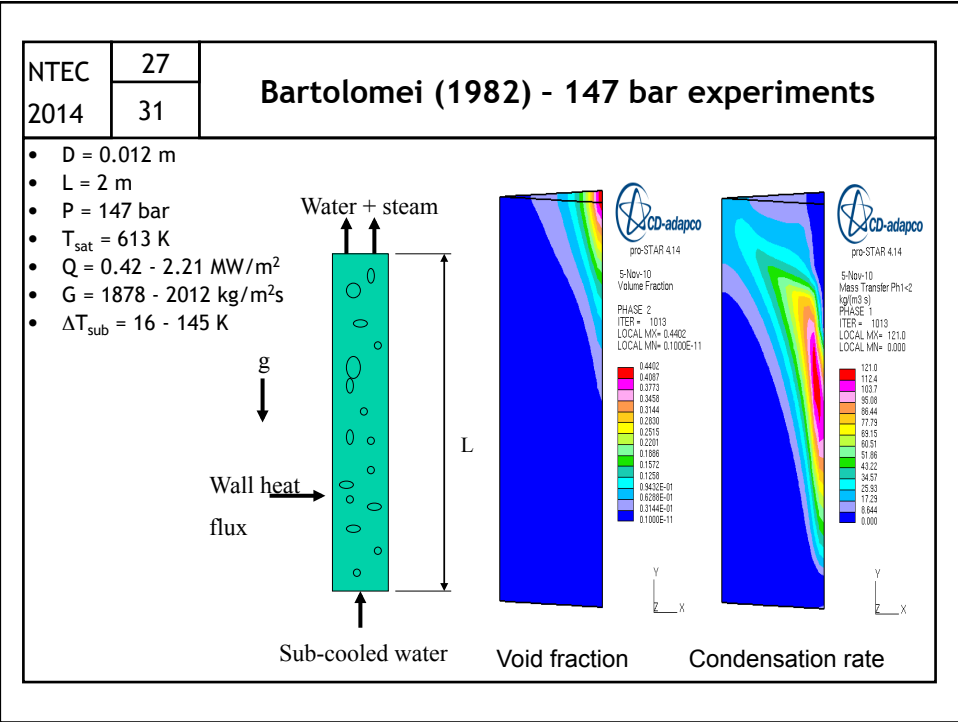
$$\dot{q}_T'' = \dot{q}_c'' + \dot{q}_q'' + \dot{q}_e''$$

Convective
heating

Quenching

Evaporation





NTEC 2014	29	Multi-component multiphase model
	31	

- General species transport equation for phase k is:

$$\frac{\partial}{\partial t}(\alpha_k \rho_k Y_k) + \nabla \cdot (\alpha_k \rho_k u_k Y_k) - \nabla \cdot \left[\alpha_k \left(D_k + \frac{\mu_t}{\sigma_Y} \right) \nabla Y_k \right] = S_k$$

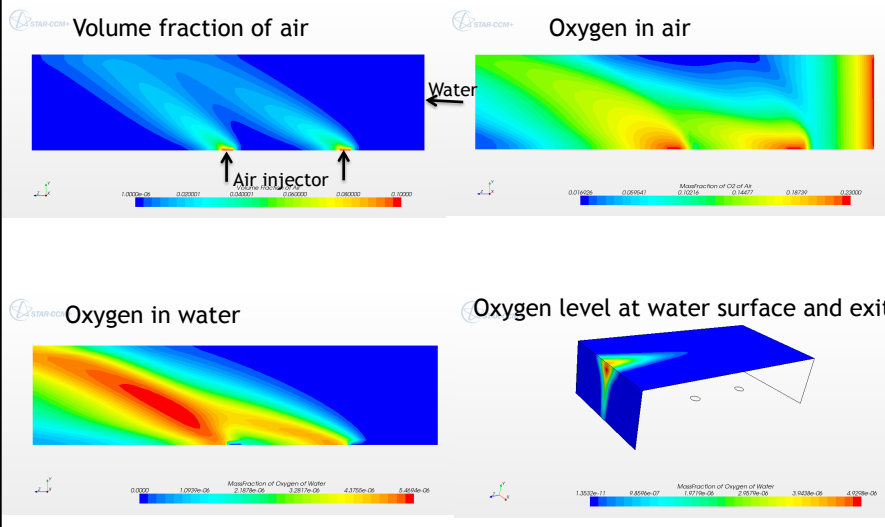
Y =mass fraction of species or other scalar quantity,

D =diffusion coefficient,

σ =Schmidt number,

S =sources.

NTEC 2014	30	Oxygen transfer in aeration tank
	31	



NTEC 2014	31	Summary
	31	
<ul style="list-style-type: none">• VOF<ul style="list-style-type: none">- Free surface flows• LMP<ul style="list-style-type: none">- Droplet flows• DEM<ul style="list-style-type: none">- Particle flows• EMP<ul style="list-style-type: none">- Particle flows- Bubbly flows- Population balance- Boiling heat and mass transfers- Interphase mass transfer		