

Demonstrating flexible operation of the TCM CO₂ capture plant

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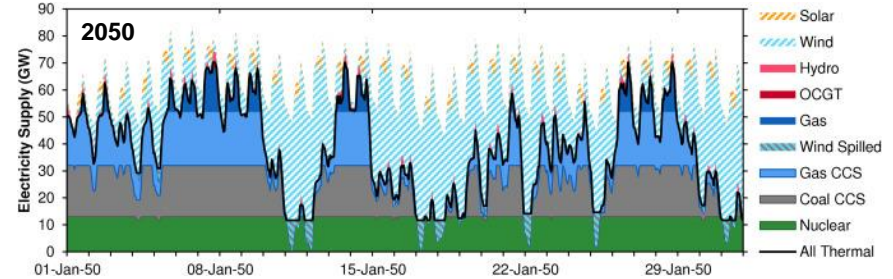
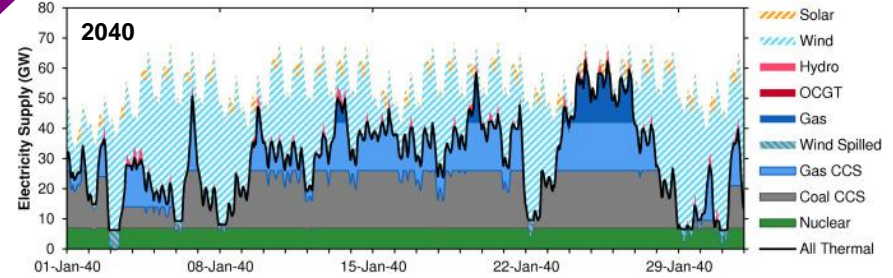
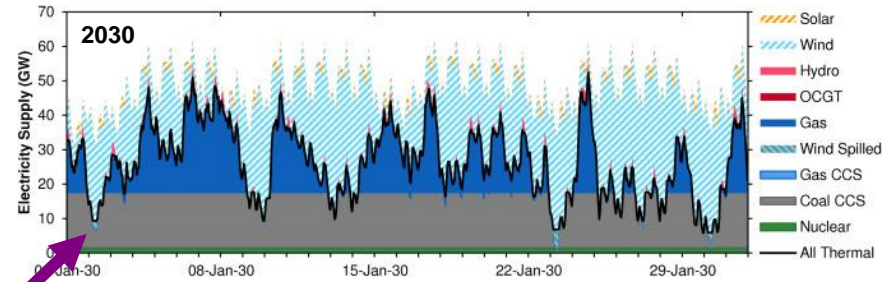
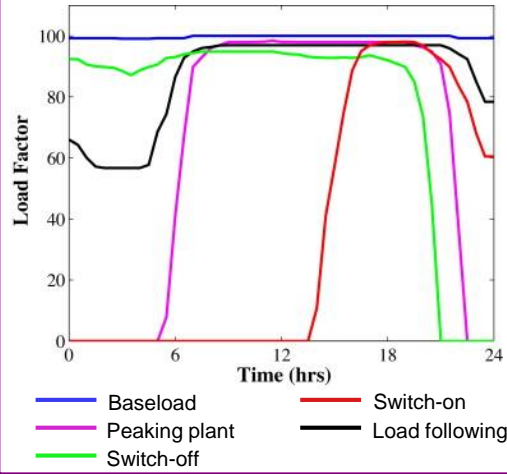
3 CO₂ Technology Centre Mongstad (TCM DA), Norway

Flexible CCS in future electricity systems

To accommodate intermittent renewables, fossil fuel power plants will need to operate flexibly.

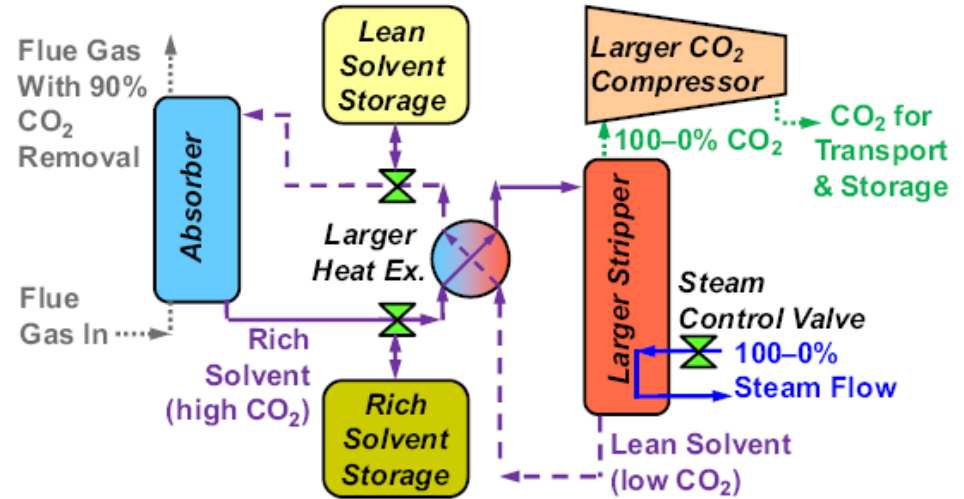
Coordinate the balance between electricity demand and CO₂ capture requirements.

Typical modes of operation for fossil fuel-fired power plants in the UK



Strategies that improve flexibility:
Solvent storage tanks

Flexible Operation Strategies

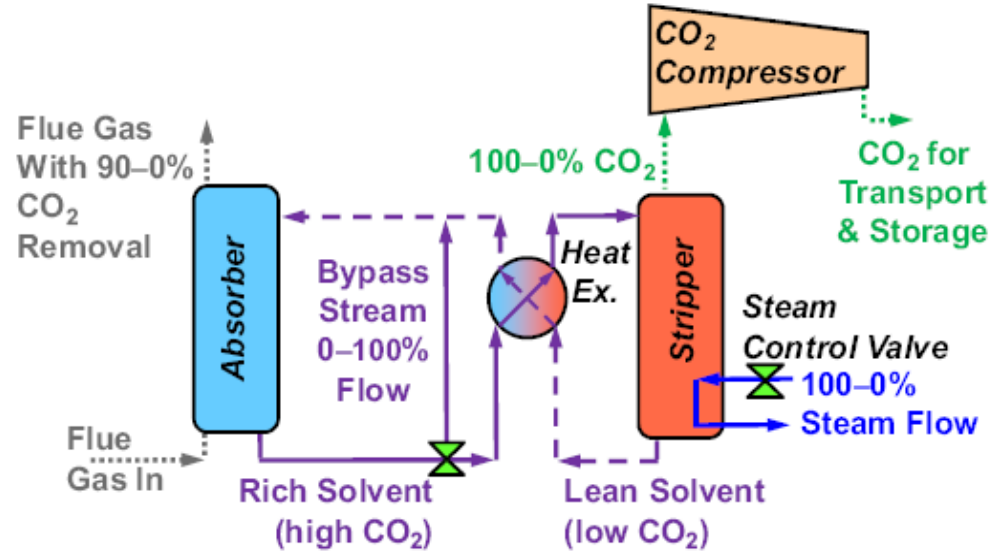


Strategies that improve flexibility:

Solvent storage tanks

Bypass system

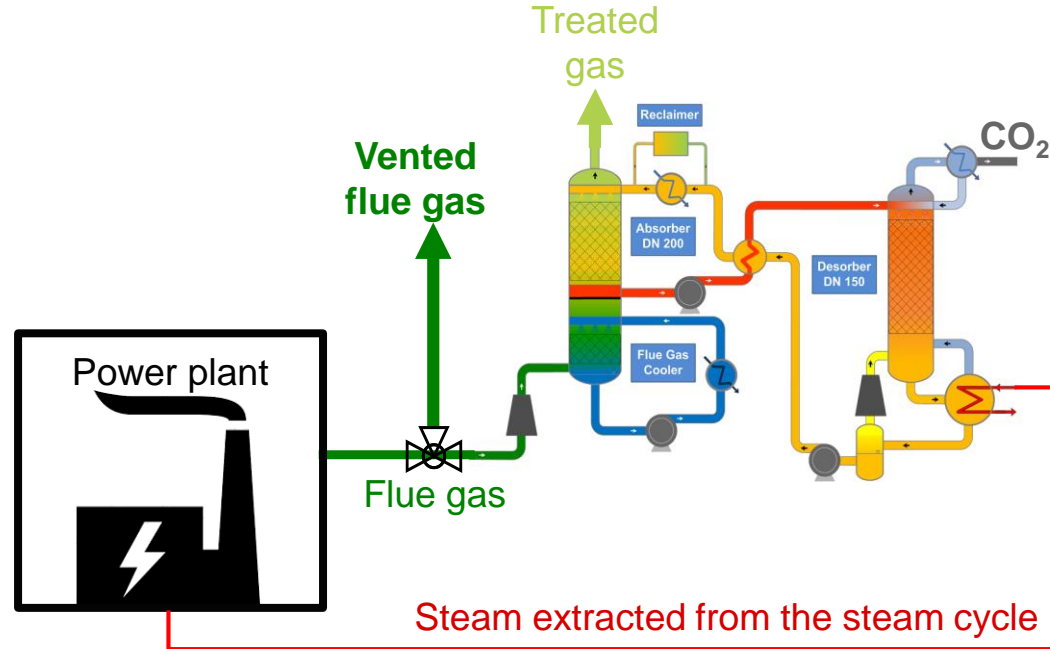
Flexible Operation Strategies



Strategies that improve flexibility:

- Solvent storage tanks
- Bypass system
- Venting system

Flexible Operation Strategies



Strategies that improve flexibility:

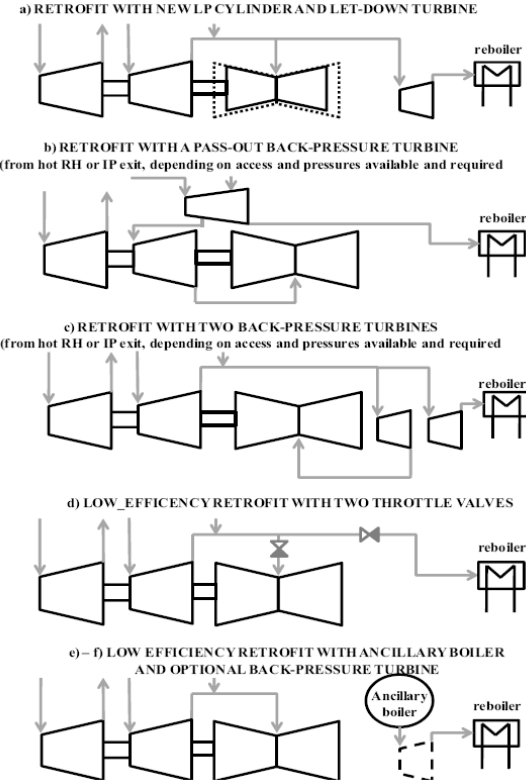
Solvent storage tanks

Bypass system

Venting system

Optimised steam cycle design

Flexible Operation Strategies



Strategies that improve flexibility:

Solvent storage tanks

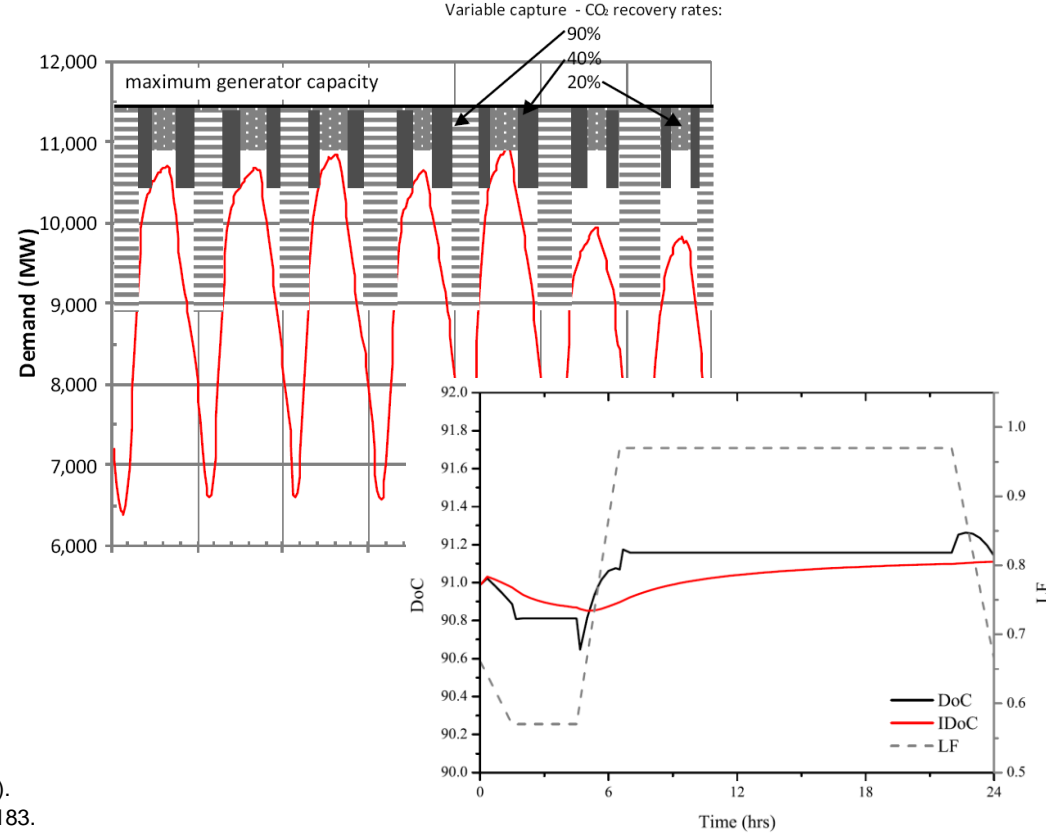
Bypass system

Venting system

Optimised steam cycle design

Load following

Flexible Operation Strategies



Wiley, D. E., Ho, M. T. & Donde, L. (2010). Energy Procedia, 4, 1893–1900 (2011).
Mac Dowell, N. & Shah, N. (2015). Computers & Chemical Engineering, 74, 169–183.

Strategies that improve flexibility:

Solvent storage tanks

Bypass system

Venting system

Optimised steam cycle design

Load following

Time-varying solvent regeneration

Time-varying solvent regeneration

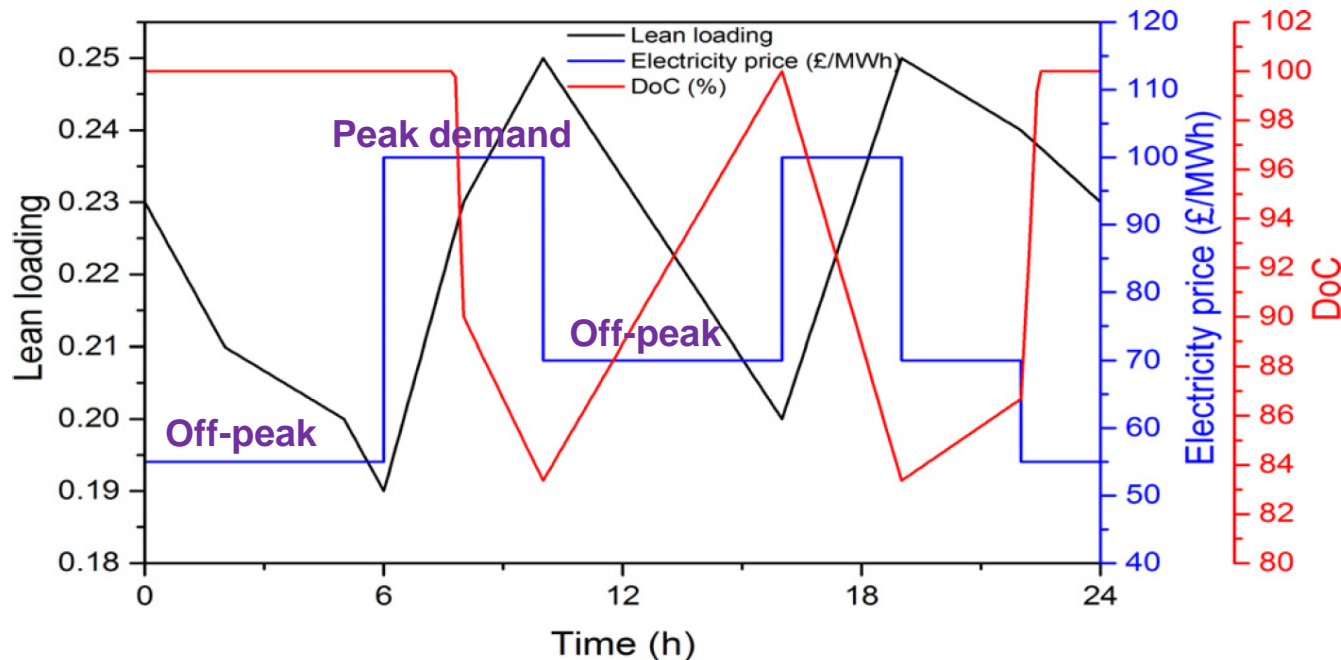
The use of solvent storage tanks involves high capital cost.

Alternatively, CO₂ can be “stored” within the amine liquid.

The **time-varying solvent regeneration** approach can be used to coordinate the DoC with electricity price/demand.

Potentially more cost effective and profitable.

Combined cycle gas turbine power plant

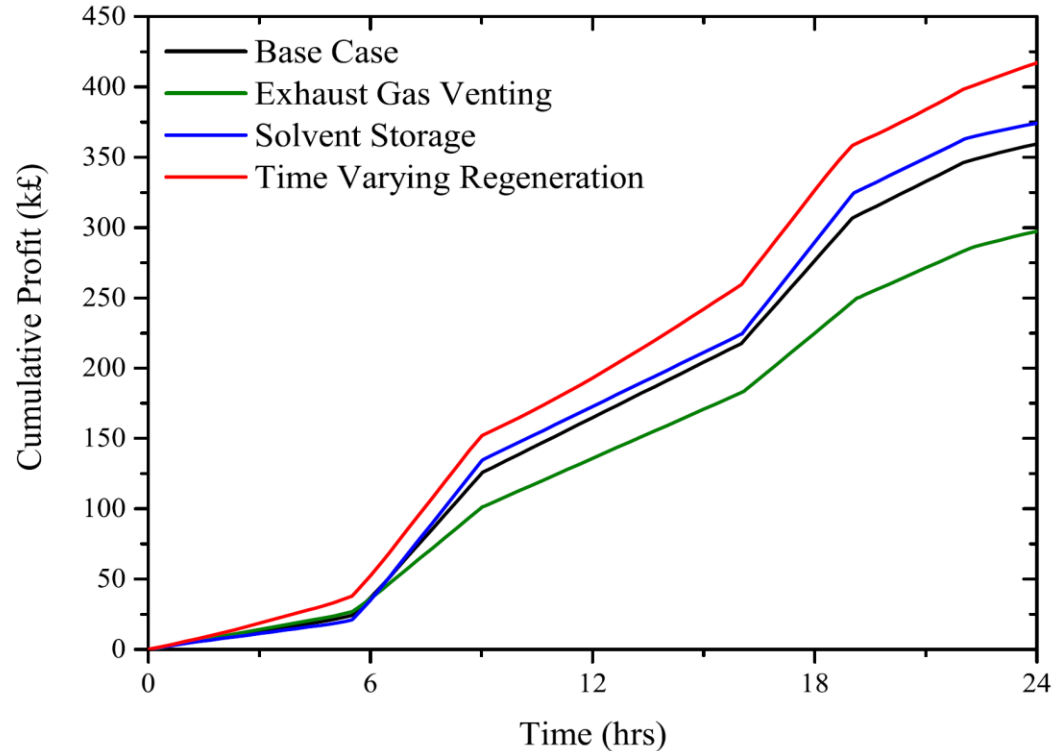


References: Mechleri, E., Fennell, P. S. & Dowell, N. M. (2017). International Journal of Greenhouse Gas Control, 59, 24–39.
Mac Dowell, N. & Shah, N. (2015). Computers & Chemical Engineering, 74, 169–183.

Time-varying solvent regeneration looks to be the most profitable strategy.

Can we actually do it?

Time-varying solvent regeneration



Mac Dowell, N. & Shah, N. (2015). Computers & Chemical Engineering, 74, 169–183.

Much of the research on flexible operation focuses on the development of operation strategies and configurations.

To design robust flexible operation strategies and process control, we need better understanding of process dynamics at larger plant scales.

This study combines experimental pilot plant testing with dynamic modelling of the TCM CO₂ capture plant.

Objective: To assess the feasibility of novel flexible operation strategies at the TCM CO₂ capture plant (time-varying solvent regeneration, variable ramp rates). Understand the effects of plant scale on the process dynamics.

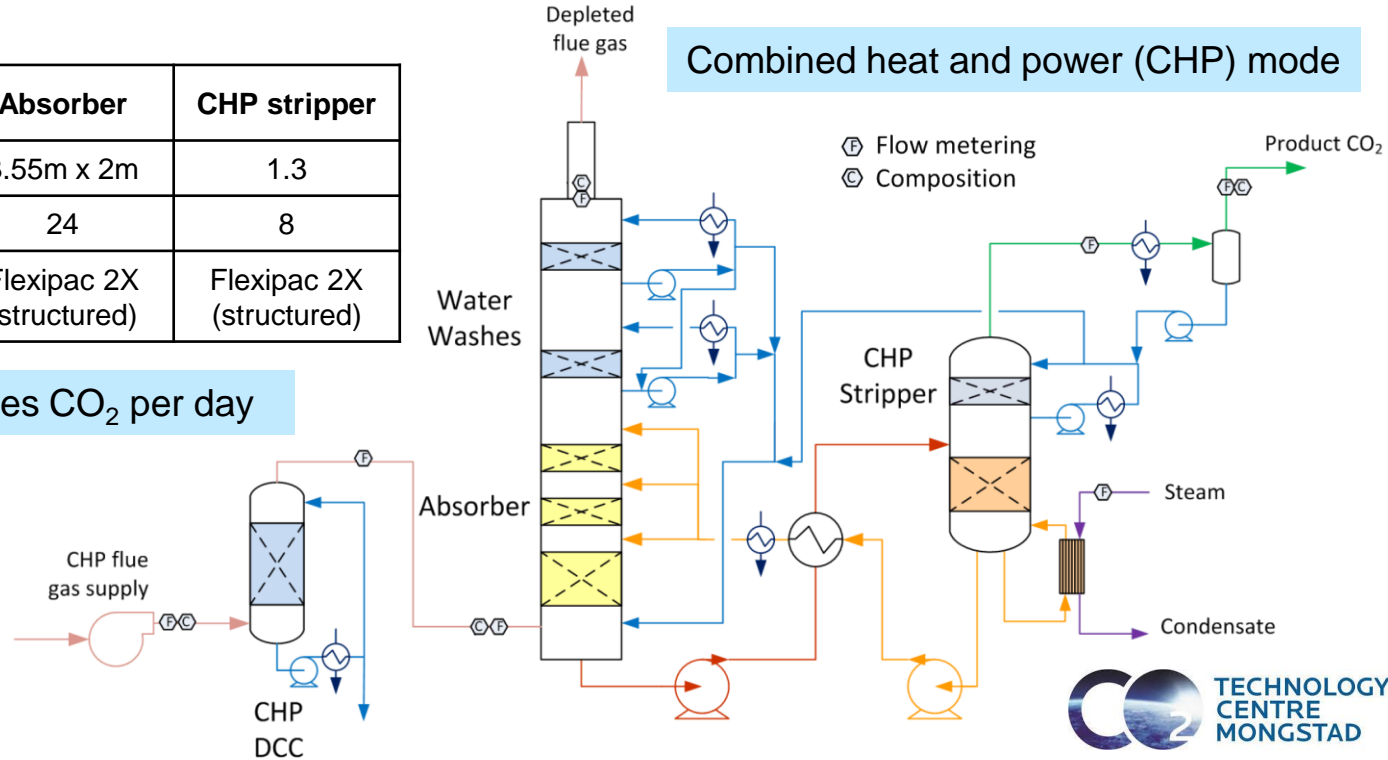
TCM CO₂ capture facility, Mongstad Norway

	Absorber	CHP stripper
Cross section dimensions	3.55m x 2m	1.3
Packing height (m)	24	8
Packing type	Flexipac 2X (structured)	Flexipac 2X (structured)

Capture capacity of 80 tonnes CO₂ per day

Flue gas component	CHP
	mole %
N ₂	78.6
CO ₂	3.6
H ₂ O	2.5
O ₂	14.4
Ar	0.9

Combined heat and power (CHP) mode



Refinery catalytic cracker (RCC) mode captures 200 t_{CO2}/day, gas CO₂ content 12.9 mol%

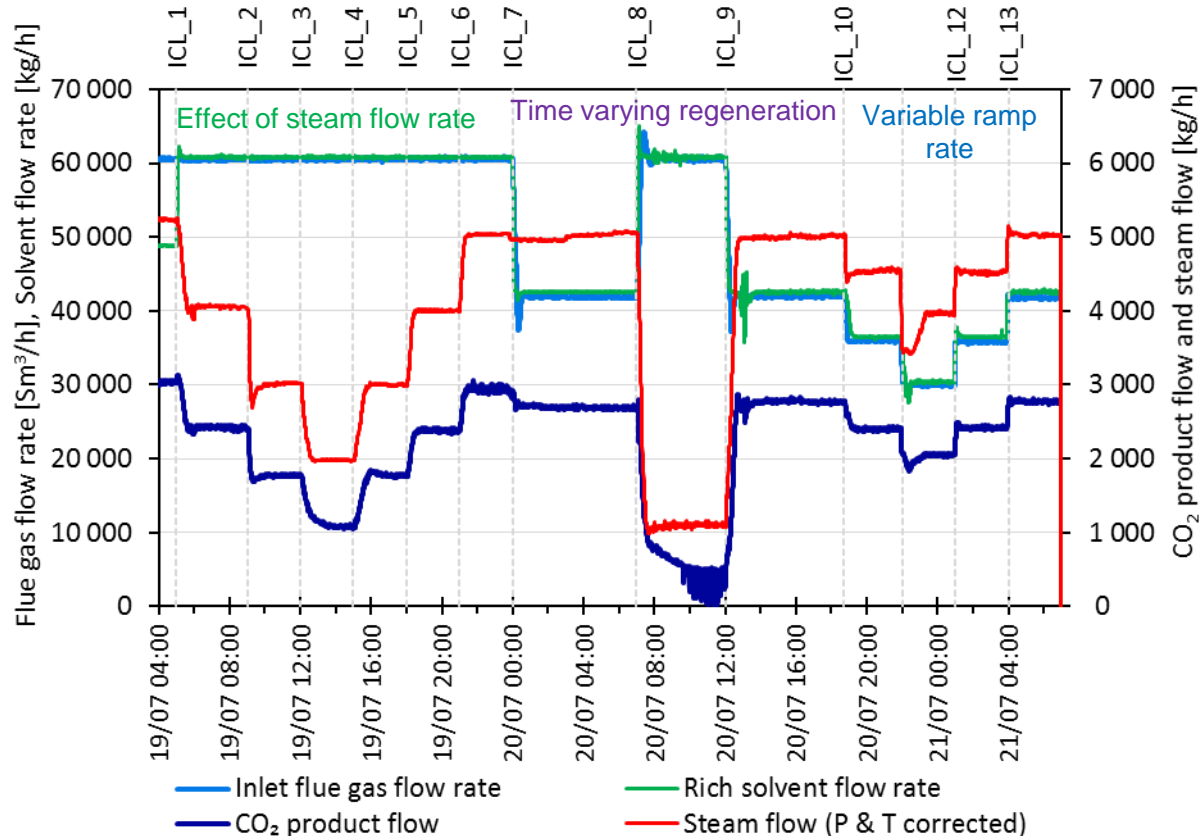
Flexible operation of the TCM CO₂ capture plant

The dynamic operation scenarios of this test campaign are:

Effect of steam flow
ICL_1 to ICL_6

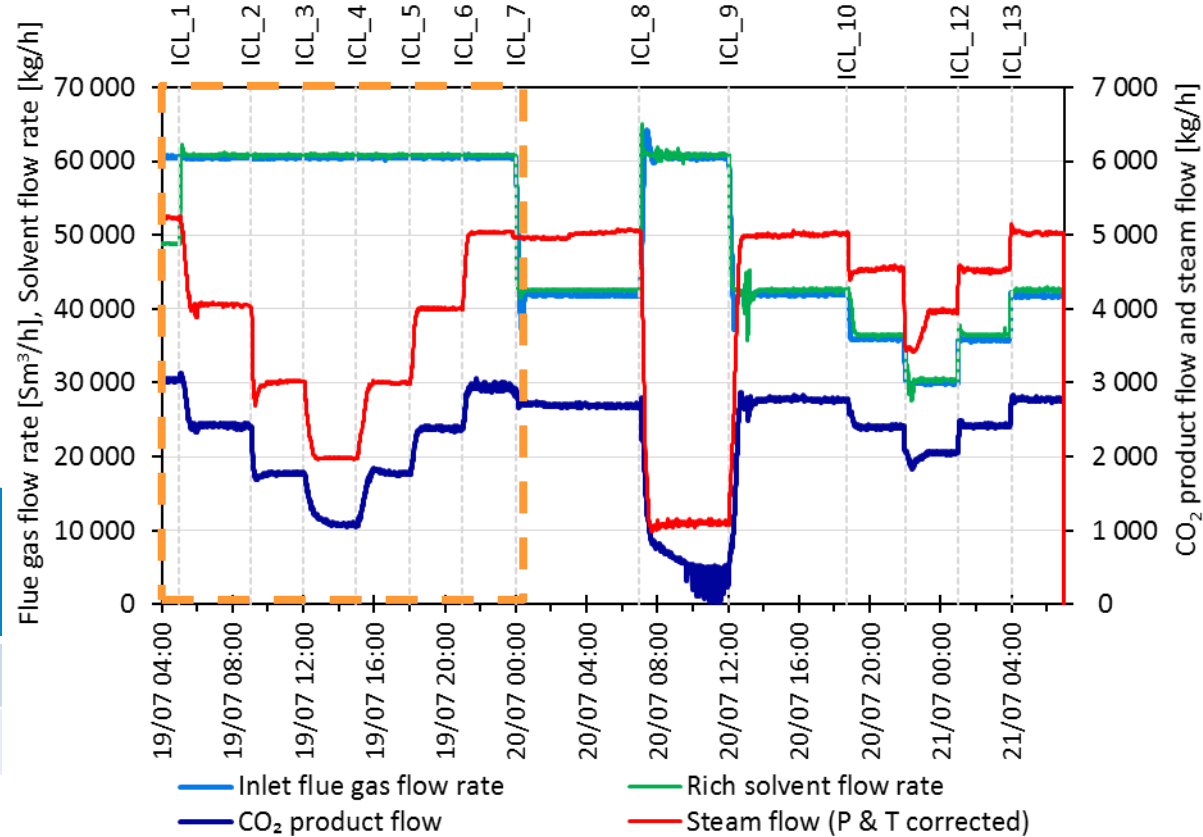
Time-varying solvent regeneration
ICL_7 to ICL_9

Variable ramp rate
ICL_10 to ICL_13



To understand the dynamics of the process, the relationship between steam flow rate and the degree of capture was establish.

Steam flow rate (kg/h)	CO ₂ capture rate (%)	Lean CO ₂ loading (mol CO ₂ / mol MEA)
2000	26.0	0.4375
5000	72.0	0.2456



Time-varying solvent regeneration

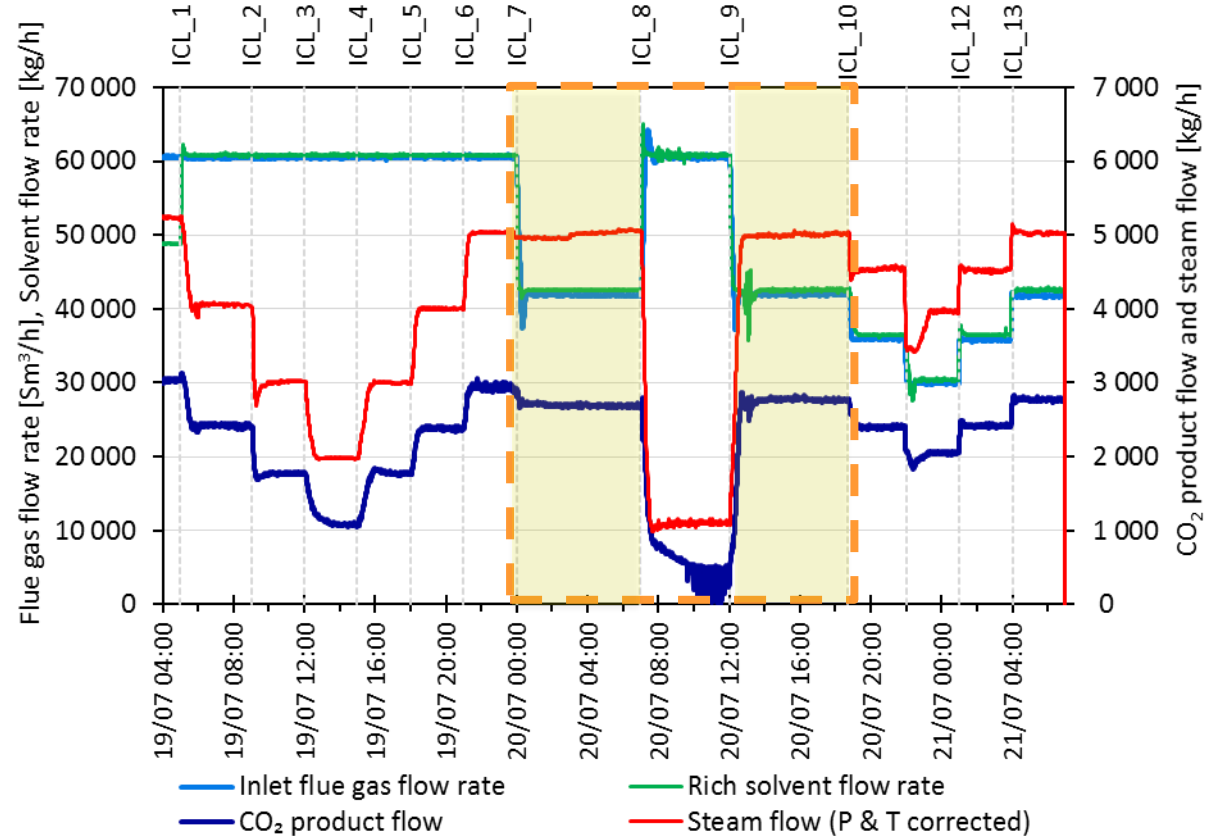
Imperial College
London

Off-peak electricity prices:

Solvent is regenerated, reducing power output → expect lower flue gas flow rates.

Increase steam flow to reboiler:

- Increases degree of capture (DoC)
- Decreases lean CO₂ loading



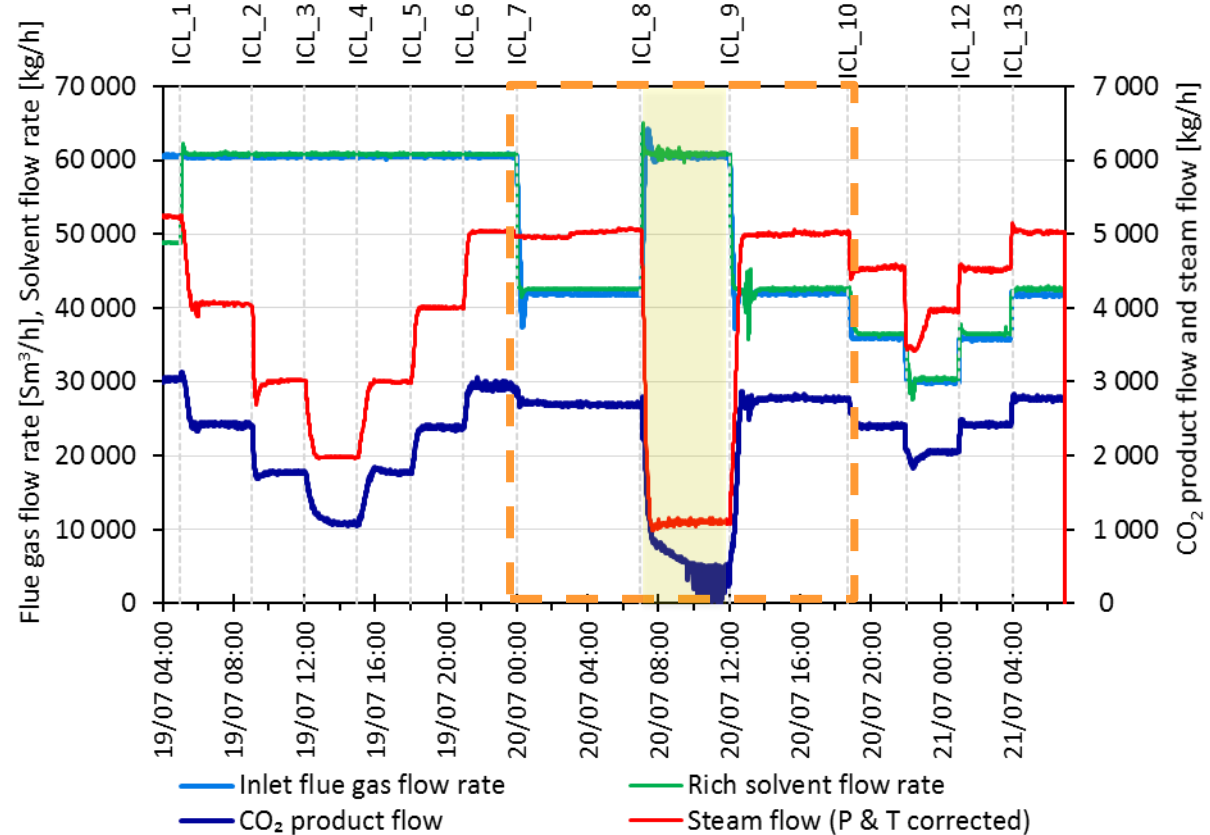
Time-varying solvent regeneration

Peak electricity prices:
accumulate CO₂ in the amine

Power output increases,
burning more fuel → higher
flue gas flow rates.

Reduce steam flow to reboiler:

- DoC reduces
- Increase in lean CO₂ loading



Time-varying solvent regeneration

Off-peak: solvent regenerated and lean CO₂ loading reduced.

Reboiler temperature: 124.1 °C

CO₂ capture rate: 89–97%

Lean CO₂ loading: 0.16 mol_{CO₂}/mol_{MEA}

Peak: CO₂ is “stored” in solvent and lean CO₂ loading increases.

Reboiler temperature: 109.5 °C

CO₂ capture rate: 14.5%

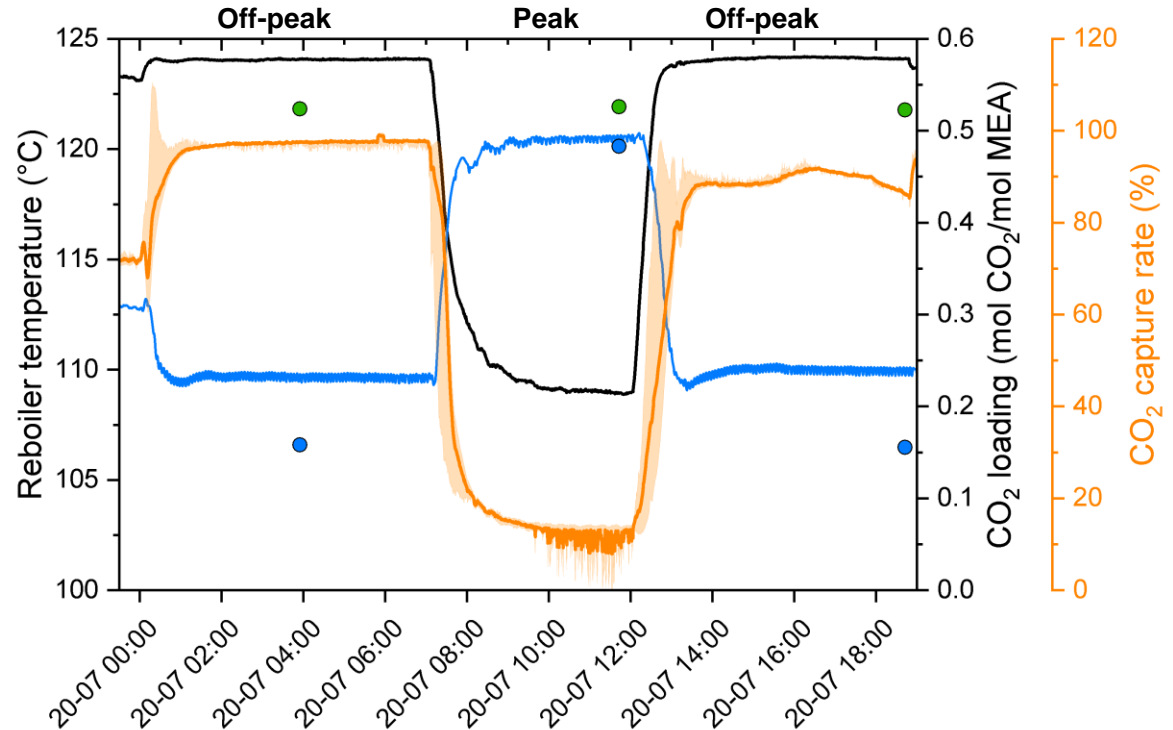
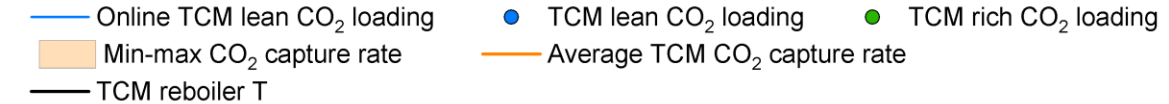
Lean CO₂ loading: 0.48 mol_{CO₂}/mol_{MEA}

Rich CO₂ Loading:

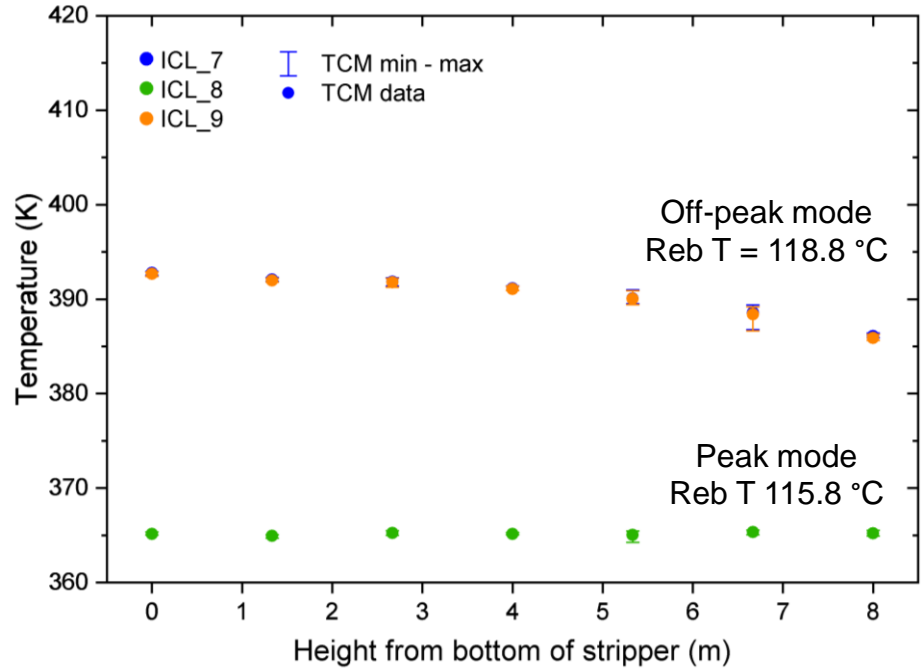
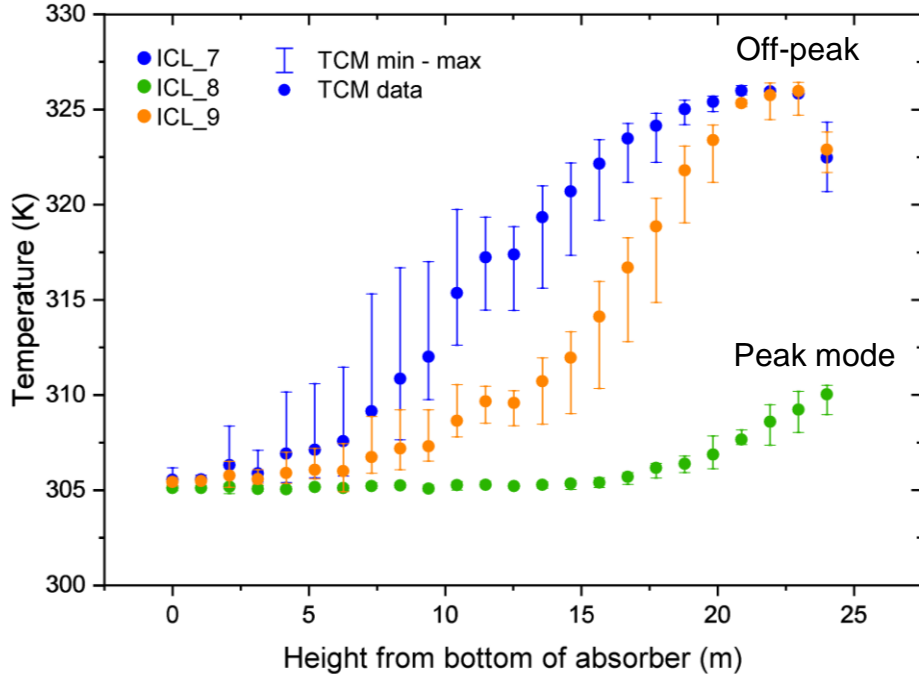
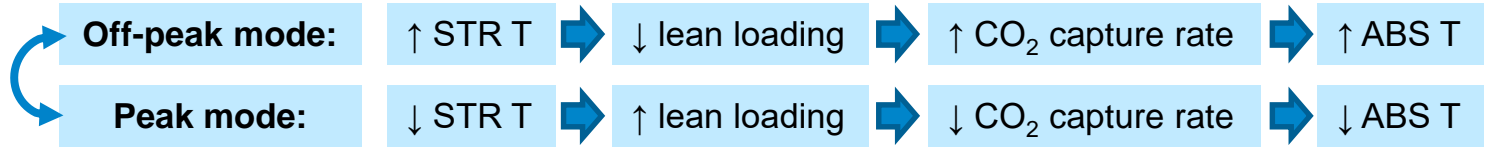
0.52–0.53 mol_{CO₂}/mol_{MEA}

Reboiler duty: 3.93–4.11 MJ/kg CO₂

Cumulative CO₂ capture rate: 66.5%



Time varying solvent regeneration



Can the CO₂ capture plant be as flexible as the power plant?

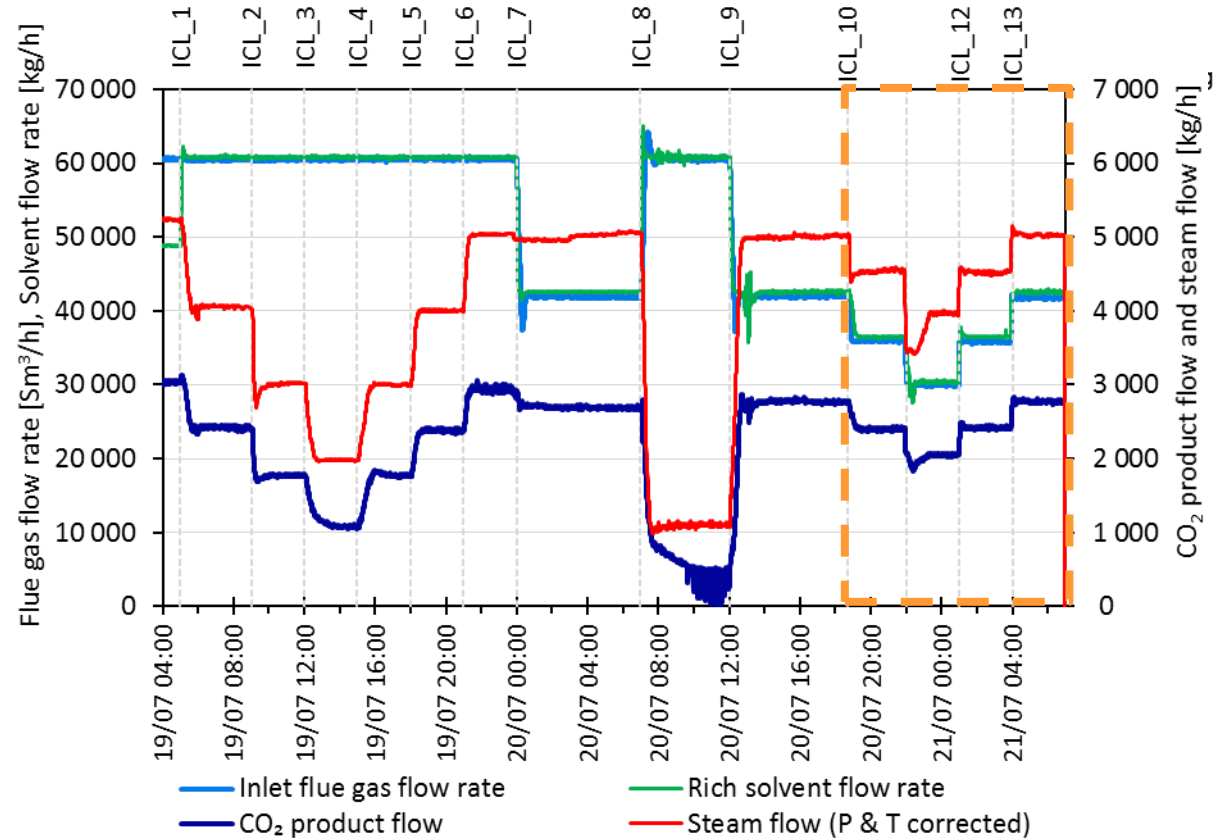
Conventional CCGT can ramp at 2–8 %P_n/min¹

Ramp rates tested:

- 1) decrease 0.6%/min
- 2) decrease 0.6%/min
- 3) increase 1.7%/min
- 4) increase 5%/min

The process control system at TCM limits ramp rate to 0.6%/min. Manual operation of blower enables ramp rates 1.7 to 5%/min.

Variable ramp rate

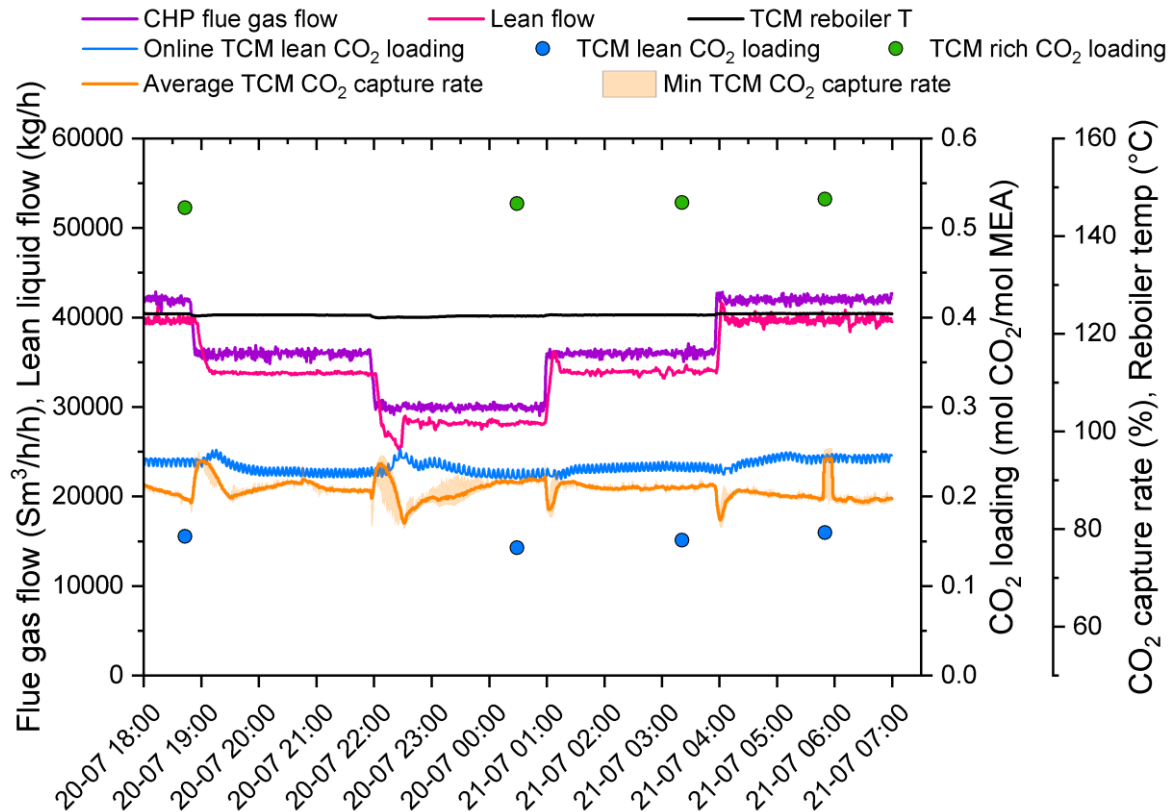


Flue gas, solvent and steam flow rates ramped simultaneously, maintaining constant L/G ratio.

CO₂ capture rate: 87–89%
Lean CO₂ loading:
 0.14–0.16 mol CO₂/mol MEA
Rich CO₂ loading:
 ~0.53 mol CO₂/mol MEA

By keeping L/G ratio constant, the CO₂ capture performance also remains constant:

- lean CO₂ loading
- rich CO₂ loading
- CO₂ capture rate



Variable ramp rate: Absorber temperature

↓ 0.6%/min ramp
FG, solvent & steam flow



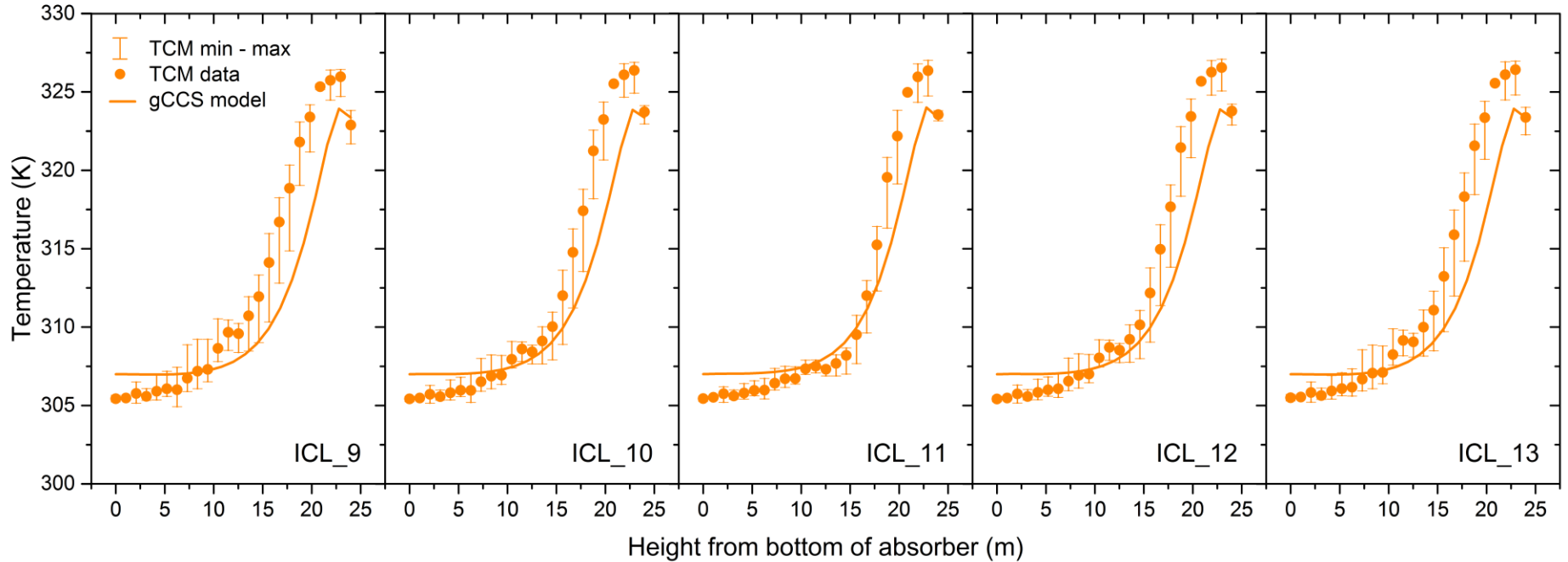
↓ 0.6%/min ramp
FG, solvent & steam flow



↑ 1.7%/min ramp
FG, solvent & steam flow



↑ 5%/min ramp
FG, solvent & steam flow



Ramp flows



L/G constant



Constant CO₂ capture rate



Constant Absorber T

Variable ramp rate: Stripper temperature

↓ 0.6%/min ramp
FG, solvent & steam flow



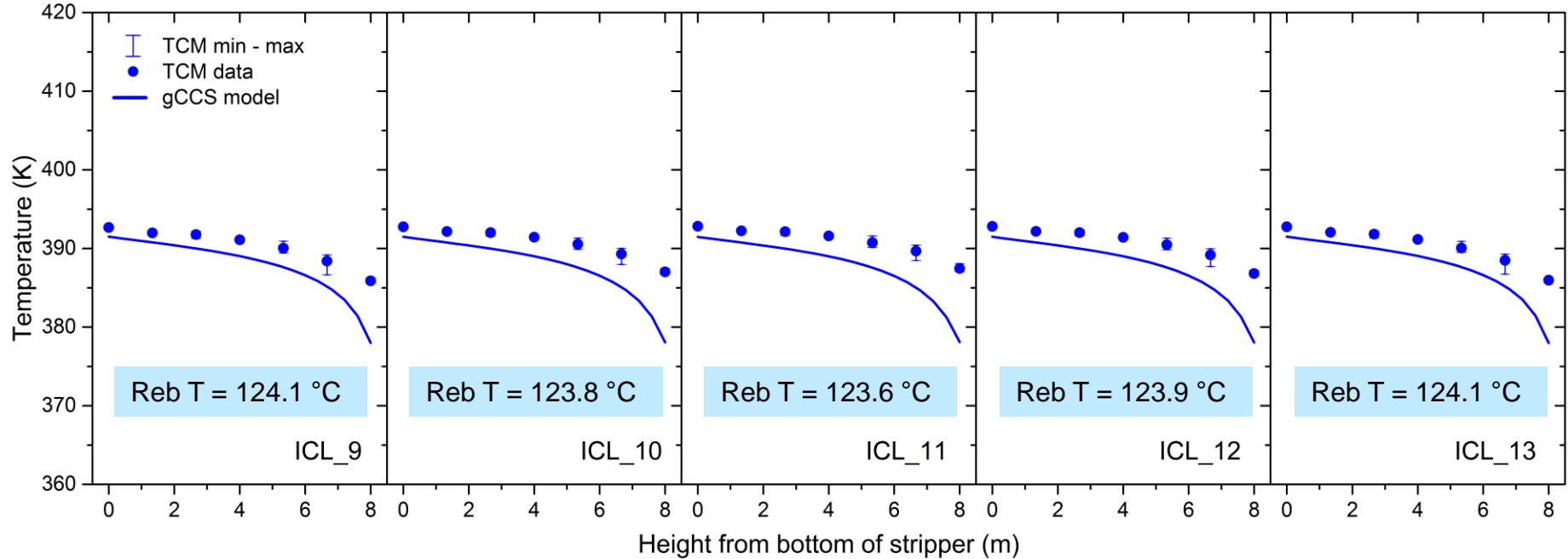
↓ 0.6%/min ramp
FG, solvent & steam flow



↑ 1.7%/min ramp
FG, solvent & steam flow



↑ 5%/min ramp
FG, solvent & steam flow



Change in steam flow rate not significant enough to result in large change in Reb T → Stripper T constant

This study demonstrates that flexible operation is technically feasible in a CO₂ capture process using MEA in the TCM CO₂ capture plant (captures 80 t_{CO2}/day in CHP mode).

Understanding the dynamics of the process is important when investigating flexible operation strategies, *e.g.*, effect of only changing steam flow rate. For example, TCM results show:

Steam flow rate (kg/h)	CO ₂ capture rate (%)	Lean CO ₂ loading (mol CO ₂ / mol MEA)
2000 ↓	26.0 ↓	0.4375 ↑
5000 ↑	72.0 ↑	0.2456 ↓

Time-varying solvent regeneration: absorption-based processes can “store” CO₂ within the amine liquid – lean loading increases from 0.16 (off-peak) to 0.48 (peak) mol CO₂/mol MEA.

Variable ramp rate: different ramp rates can be applied in succession. By maintaining a constant L/G ratio, CO₂ capture performance (capture % and loading) will remain constant

Key characteristics found to limit flexibility

Stabilisation time: Need to allow sufficient time to stabilise the plant before changing to new process conditions.

Transition time: For step changes and rapid ramp rates to new set-point conditions, actual process conditions do not transition immediately, it takes time to reach final set-point conditions. This time varies with parameter & size of the change.

Magnitude and speed of process parameter change: Rapid and large process parameter changes tend to be avoided at TCM to prevent inverse responses and plant instability (observed in previous test campaigns).

Process control system: Designed for steady state operation. Found to be the key factor that limited ramping capabilities. This is an important area for future work.

Plant flexibility is a function of the **scale** of the plant and **volume of solvent inventory**.

Further research challenges

Further work studying plants at other different scales → larger scale, slower dynamics

- Develop a correlation between plant scale and dynamic CO₂ capture performance.
- PACT 1 t_{CO2}/day → Brindisi plant 60 t_{CO2}/day → TCM 80 t_{CO2}/day

Solvent development/design

- Improve fluid flow properties to ensure adequate solvent distribution over the packing.
- Higher working capacities (i.e., more moles of CO₂ per mole of liquid absorbent).

Tool development

- Improve accuracy of commercial software to better model dynamic physical behaviour
- Liquid measurement instruments that **accurately** measure CO₂ loading online.
- Process control strategies that improve operability during flexible operation (e.g. to achieve faster ramp rates).

Integrate flexible CO₂ capture processes into energy system models to identify the value of flexible CCS.